Consumer and Corporate Affairs Canada

Consomn: tion et Corporation Canada

SPG-246

Consumer Standards Directorate

Direction générale des normes

OTTAWA, June 14, 1978

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SPECIAL APPROVAL

Granted to: Shell Canada Resources Limited,

Burnt Timber Cas Plant,

Cremona, Alberta.

Attention:

Mr. William Evans. Project Manager.

Subject:

10" XS Non-Standard Orifice Meter Run with

Auxiliary Devices.

Special Approval has been granted by the Legal Metrology Branch to Shell Canada Resources Limited for the use of a 10" MS non-standard orifice run at Cremona, Alberta, for the sale of gas to Alberta Gas Trunk Line Co. Ltd. Billing shall be based upon the accumulated flow as indicated on the recorder

Details of the meter and auxiliary attachments for the meter run 10FE-12 are as follows:

1. Orifice Meter:

Manufacturer

Serial number Maximum working pressure, psi Schedule

Flange rating Nominal pipe size Inside pipe diameter Orifice diameter Beta (d/D) ratio. Pressure taps

Maximum flow

Robinson Orifice Fitting Co.

77-6131-2

PECO Robinson "E"

1480 XS

ASA 600

lo"

9.750"

5.625"

0.5769

Plange

4,901,460 SCFH

2. Auxiliary Attachments

(a) Chart Recorder: Manuafacturer

Model. Sorial Number Number of pens Foxboro Co. Ltd., 12R M = 3058013

(i) Temperature: Class 1-A, fully temperature compensated.

Range: 0-100°C.

S.S. capillary length 25 ft. armoured.

Immersion length 6 in.

Á

(ii) Static Pressure: Range: 0-10 MPa

Class: S.S. Helical

(iii) Differential

Pressure:

Range: 0-50 kPa

Class: 37

(b) Chart:

Manufacturer Type number

Foxboro 898418

12" Circular

Scale or Chart Range: Temp: 0-100 Lin.

Static

press:

0-100 Lin.

Diff.

press: 0-10\h

The orifice meter constants shall be calculated in accordance with the AGA Gas Measurement Committee Report No. 3 (1969). However, since the facility is operating atilizing S.I. units, these readings must first be converted to English Units using recognized conversion factors (see CGA SI Conversion Factors for Canadian Gas Industry) for flow rate calculations.

This approval is contingent upon the metering system conforming to the requirements delineated in the applicable Sections of Part VIA and Part II of the Departmental Instructions for the Inspection of Cas Meters and Auxiliary Devices.

A procedure for field testing of this system is outlined in Appendix A attached. 21.

> D.L. Smith, Chief,

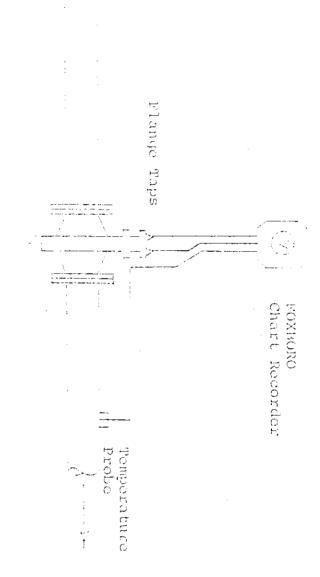
Electricity & Gas Division.

c.c. Mr. L. Hewitt, D.I., ESG, Cargary.

Mr. E. M. Bailin, Project Madager, The Ralph M. Parsons Company Limited.

Mr. J. T. Meers, Engineering Department, E.A. Kutryk Industries Limited.

ORIFICE MET: A INSTALLATION AT BURNT TIMBER GAS PLANT, CREMONA, ALBERTA



APPENDIX "A"

Re: Special Approval SPG-246

June 14, 1978

Field Test Procedure for Verification of Shell Canada Resources Limited Orifice Meter Installation at Burnt Timber Gas Plant, Cremona, Alberta.

Field Test Procedure

(A) Primary Elements:

The orifice plate and the installation shall be examined and dimensional measurement made to verify the conformity with Specification No. 7 for Approval of Type of Orifice Gas Meters and their Installation.

- (B) Secondary Elements:
 During the verification tests it is important for the flow conditions to be stable.
 - 1. For verification tests <u>simulate</u> the flow conditions by applying appropriate temperature, and static and differential pressures, which can be held constant for the duration of the test.
 - 2. Insert the three (3) parameters* obtained above into the following calculated orifice gas equation example, which is based upon the existing Shell Canada Resources system.

EXAMPLE:

CONDITIONS AT METER

VALUE OF FACTOR

Meter equipped with Flange Taps. d = diameter of orifice = 5.625 in.

D = internal dia, of meter tube = 9.750 in.

Determination of the Basic Orifice Factor, F_b : For the non-standard pipe size with inside diameter of 9.75" the F_b is calculated in accordance to equation (25), section (Bl2) of Appendix "B", AGA Report #3.

 $F_b = 6849.14$

Static pressure obtained upstream of meter.

- * Average differential (at normal flow), $h_w = 132.774 \text{ in. W.C.}$
- * Average static pressure, p_f = 972.7 psia (958 psig)
- Standard atmospheric pressure = 14.7 psia = $5.625 \div 9.750 = 0.5769$

$$\sqrt{h_{\rm w}p_{\rm f}}$$
 = pressure extension (average) = $(132.774 \times 972.7)^{\frac{1}{2}} = 359.37$

For $\beta = 0.5769$ and D = 9.750; b = 0.0371

$$F_r = 1 + (0.0371 \div 359.37) = 1.001$$
 $F_r = 1.0001$

Differential ratio,
$$h_w \div p_f = 132.774 \div 972.7 = 0.1365 \quad Y_1 = 0.9983$$

$$P_b$$
 = base pressure = 14.7 psia F_{pb} = 1.0020

$$T_b = temperature base = 60°F$$
 $F_{tb} = 1.000$

*T_f = flowing temperature=93°F;
$$\left(F_{tf} = \sqrt{\frac{60+460}{T_f+460}}\right)$$
 F_{tf} = 0.9697

$$G = \text{specific gravity} = 0.61$$
 $F_g = 1.2804$

Supercompressibility factor for 958 psig and
$$93^{\circ}$$
 F: $_{pv}^{=}$ 1.0645

Manometer factor:
$$F_{m} = 1.0000$$

Area Factor,
$$F_a$$
 and Location factor, F_ℓ are assumed to be unity (1.000)
$$F_a = 1.0000$$

$$F = 1.0000$$

Orifice constant, C', corresponds to the expression:

$$C' = F_b \times F_r \times Y_l \times F_{pb} \times F_{tb} \times F_{tf} \times F_g \times F_{pv} \times F_m \times F_a \times F_{\ell}.$$

Then,
$$C' = 6849.14 \times 1.0001 \times 0.9983 \times 1.0020 \times 1.0000 \times 0.9697 \times 1.2804 \times 1.0645 \times 1.0000 \times 1.0000 \times 1.0000 = 9056.0$$

For an average pressure extension, $\sqrt{h_w p_f} = (132.774x972.7)^{\frac{1}{2}} = 359.37$, the flow rate would be

 $Q_h = C' \sqrt{h_w p_f} = 9056.0 \times 359.37 = 3,254,455$ cu. ft. per hr. The above equation, $Q_h = C' \sqrt{h_w p_f}$, can be converted to an equation where all three parameters are included in the solution of the flow equation, namely,

where Q_h = rate of flow in cu. ft. per hr. at base conditions, C' = orifice flow constant as designated in AGA Report No. 3

$$C'' = \frac{C'}{F}$$

 $F_{+f} = gas$ flowing temperature factor

 p_f = absolute static pressure in psia

 $h_{_{\mathbf{W}}}$ = differential pressure in inches of water.

Equation (1), above, can be used to calculate the flow at any set of stable operating conditions.

Note: Shell Canada Resources base temperature and pressure is 60°F and 14.7 psia, respectively.

The verification tolerance is in accordance with Departmental Instructions, Part VIA, section 4.